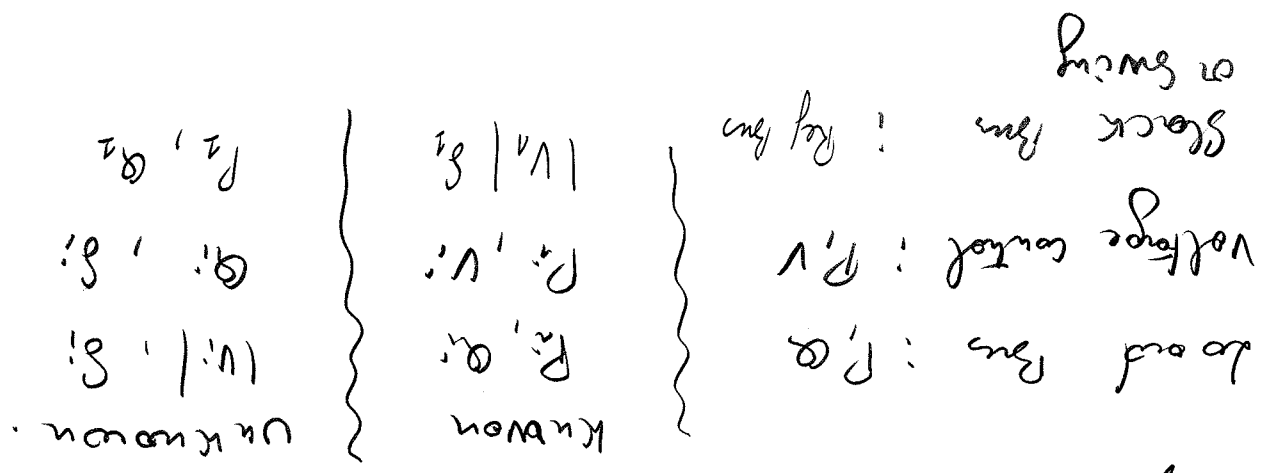


1) Power systems are categorized into 3 Powers system types -



2) only one slack or swing bus and, as it's taken as reference bus. $|V_1| = 1 pu$ and $\delta = 0^\circ$.

3) From STF, P and Q expression are

$$P_i = \sum_{n=1}^N |V_i V_n| \cos(\theta_{ik} + \delta_k - \delta_i)$$

$$Q_i = \sum_{n=1}^N |V_i V_n| \sin(\theta_{ik} + \delta_n - \delta_k)$$

4) Newton-Raphson and Gauss-Seidel are mainly used. Both method are used to solve STF equations which are non linear algebraic equations start to initial value and iterative successive approximation -

Exor 1/1

↓ set of symmetrical components

- Positive sequence - noted V_1 or V_2
- Negative " - noted V_1 or V_2
- Zero sequence - no tnd V_0 or V_0

$$\begin{bmatrix} V_1 \\ V_2 \\ V_0 \end{bmatrix} = \frac{1}{\sqrt{3}} \begin{bmatrix} 1 & a & a^2 \\ 1 & a^2 & a \\ 1 & 1 & 1 \end{bmatrix} \begin{bmatrix} V_A \\ V_B \\ V_C \end{bmatrix}$$

with

$$\begin{cases} a = 1 \angle 120^\circ = -0.5 + j0.866 \\ a^2 = 1 \angle 240^\circ = -0.5 - j0.866 \\ a^3 = 1 \angle 360^\circ = 1 + j0 \end{cases}$$

$$V_0 = \frac{1}{\sqrt{3}} \begin{bmatrix} 18 \angle 0^\circ \\ + 10 \angle -132^\circ \\ + 15 \angle 90^\circ \end{bmatrix} = 18 + j0 = -6.7 - j7.43 = 0 + j15$$

$$\frac{1}{\sqrt{3}} [11.3 + j7.57] = 3.71 + j2.58$$

$$V_0 = 4.53 \angle 33.83^\circ$$

$$V_1 = \frac{1}{\sqrt{3}} \begin{bmatrix} 18 \angle 0^\circ \\ + 10 \angle -132^\circ \\ + 15 \angle 90^\circ \end{bmatrix} = 18 \angle 0^\circ = 18 + j0 = 9.78 - j2.08 = 15 \angle 33^\circ = 12.40 + j15 \angle 33^\circ$$

$$V_1 = 13.6 - j3.193$$

$$V_2 = 13.96 \angle -13.22^\circ$$

with $V_1 = 0.64 + j0.67$
 $V_2 = 0.9266 \angle 46.32^\circ$

3/

$$S_{3\phi} = V_a I_a^* + V_b I_b^* + V_c I_c^* = (P_a + jQ_a) + (P_b + jQ_b) + (P_c + jQ_c)$$

$$= 18 \angle 0^\circ * 180 \angle 110^\circ = 3240 \angle 110^\circ = 3194 + j562,6 \text{ VA} \\
= 10 \angle -132^\circ * 250 \angle 100^\circ = 2500 \angle -32^\circ = 2120,12 - j1325,18 \text{ VA} \\
= 15 \angle 90^\circ * 200 \angle -50^\circ = 3000 \angle 40^\circ = 2298 + j1928,4 \text{ VA}$$

$$\underline{7609 \text{ W} + j1176,2 \text{ VAR}}$$

$$S_{3\phi} = P + jQ = 7609 \text{ kW} + j1176,2 \text{ kVAR}$$

with $P_a = 3191 \text{ W}$ and $Q_a = 562,6 \text{ VAR}$
 $P_b = 3191 \text{ W}$
 $Q_b = 1176,2 \text{ VAR}$

4) $|I_{lg}| = 315 \text{ A}$

with I_0 some calculation made for V_0 .

~~$I_0 = 264,7 \text{ A}$~~
 Software calculation???

~~$|I_{lg}| = 614,1 \text{ A} \rightarrow |V_n| = 614,1 \text{ A} \times 10 = 6,14 \text{ kV}$~~

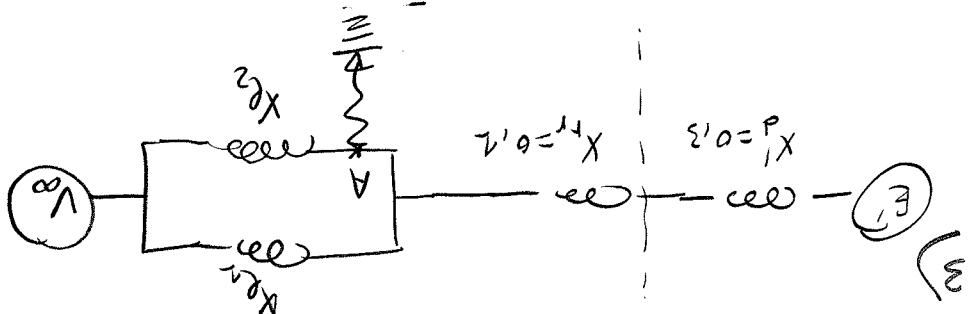
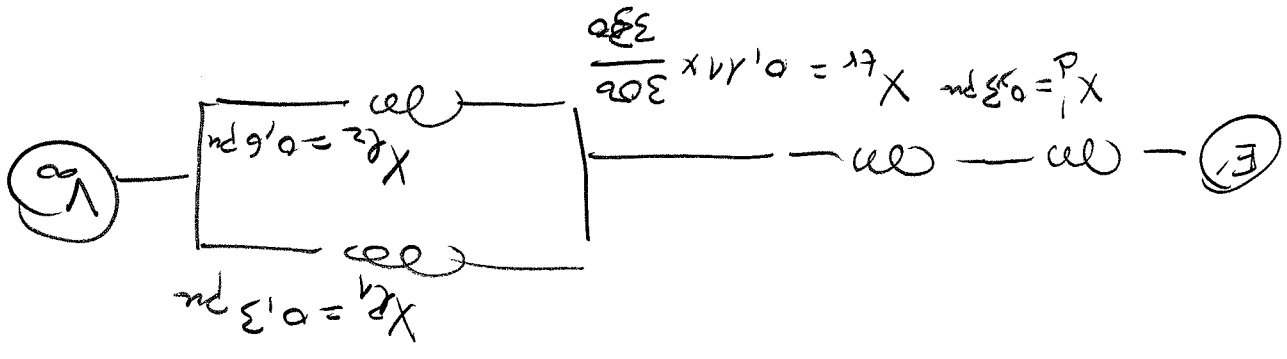
$|V_n|$ Neutral voltage relative to ground.

$$I_n = 177,26 - j31,26 + [-43,4 - j246,2 + 128,56 + j153,2]$$

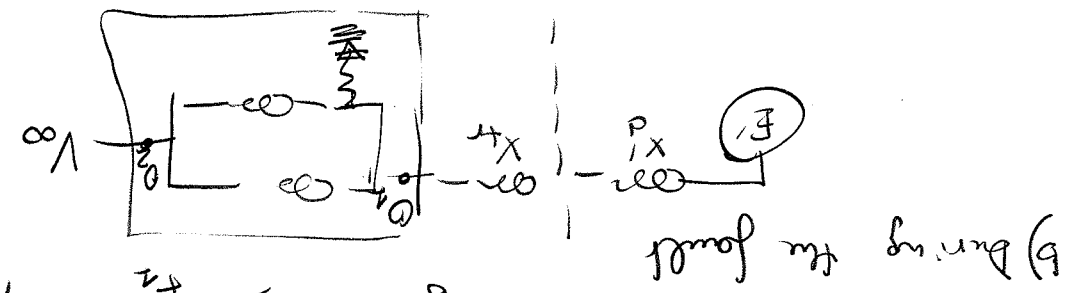
$$\Rightarrow V_n = 2,9 \text{ kV} \angle -25,34^\circ$$

1 - X_D : synchronous direct gearance

X'_D : synchronous direct transient gearance.

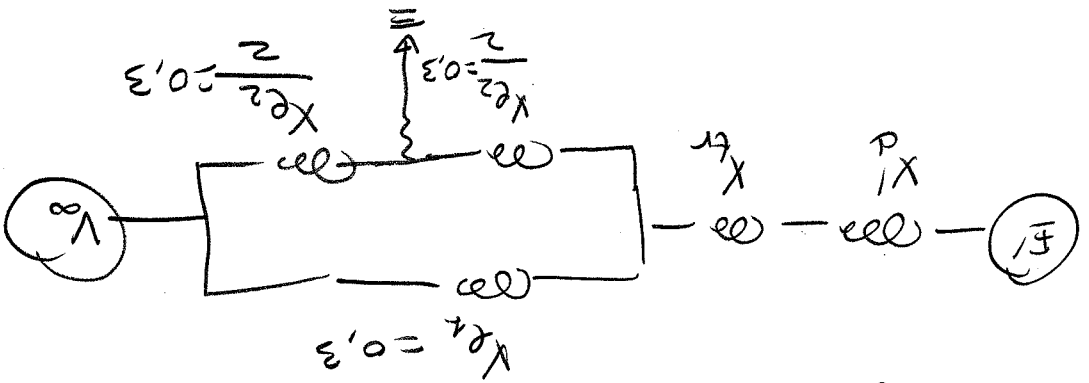
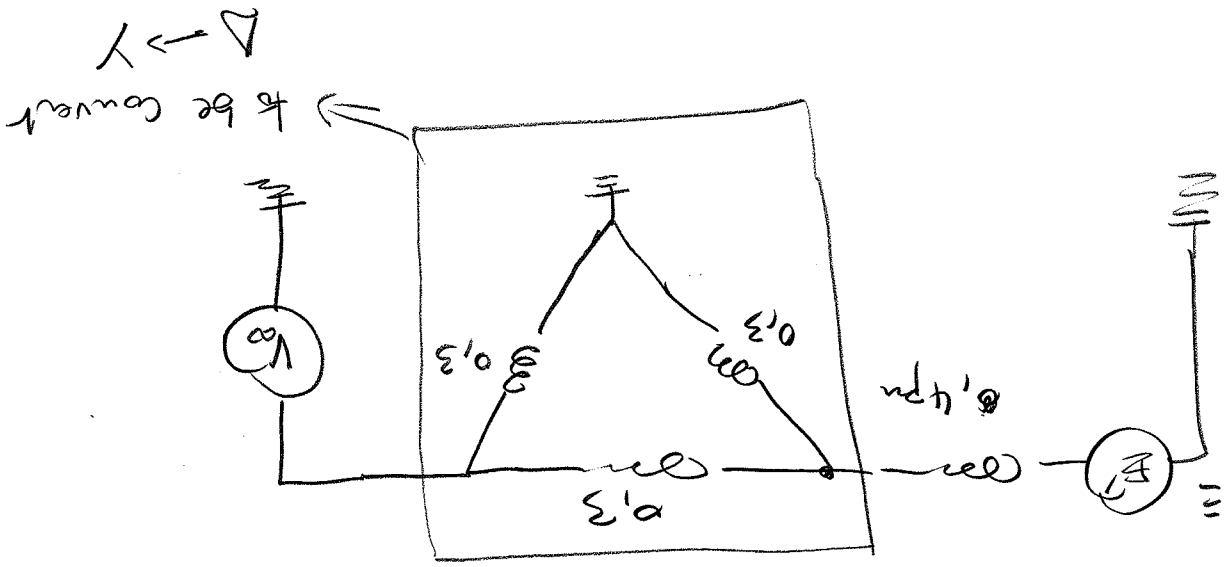


2) Just before fault
 $X_{fa} = 0.12 + \frac{0.3 \times 0.6}{0.3 + 0.6} = 0.16 \text{ pu}$
 including $X'_D \Rightarrow X_{fa} = 0.16 \text{ pu}$



3) During the fault
 from 0.16 to 0.14 the impedance is considered

4) after the fault, with X_2 removed
 $X_{fb} = 0.12 + 0.3 = 0.14 \text{ pu}$ considering X'_D
 $X_{fb} = 0 \Rightarrow X_{f2} = 0$

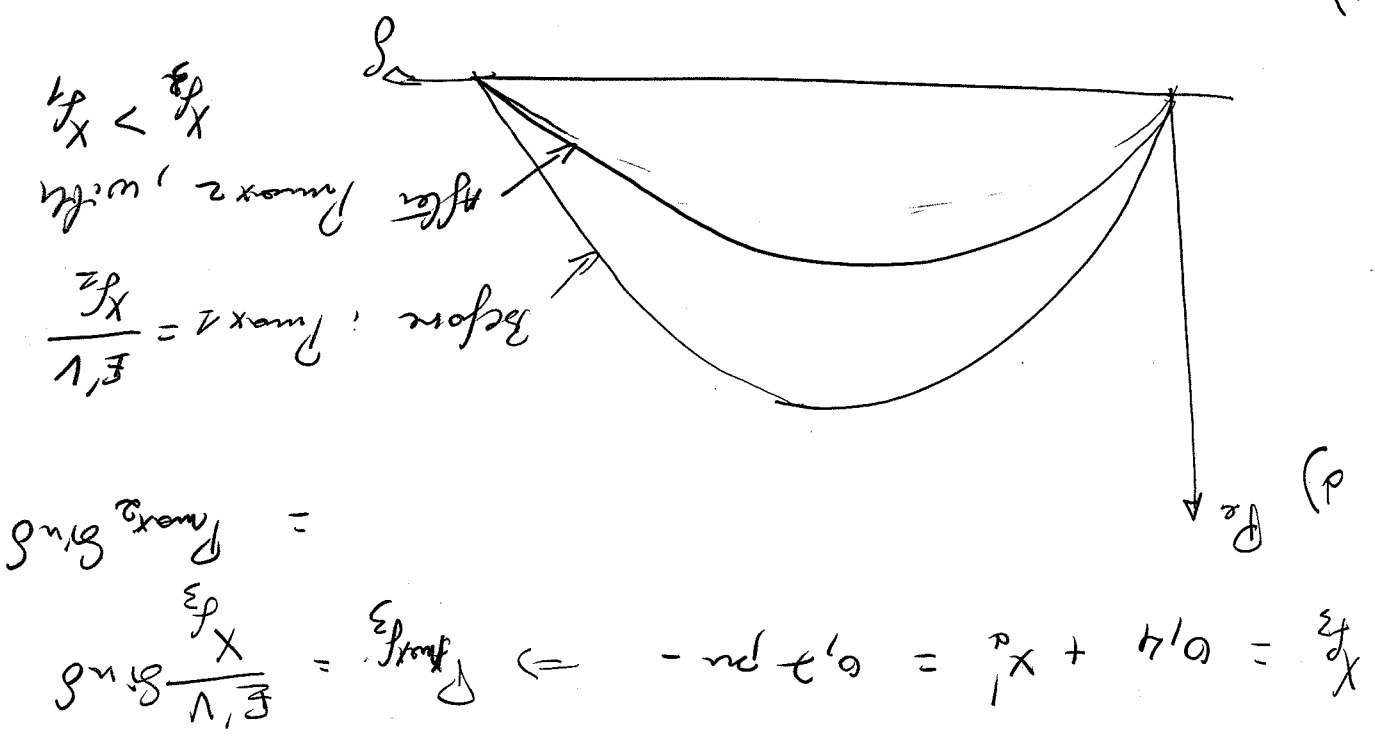


b)

c)

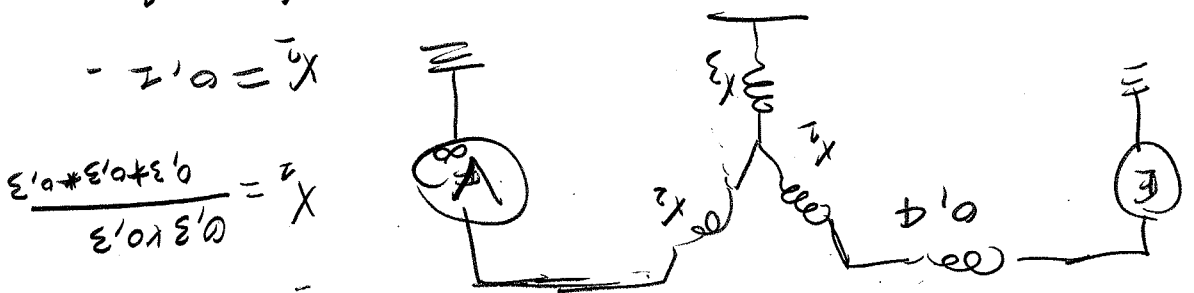
fault takes place at the middle of X_2

d)



d)

Application theorem of Kennedy $\Delta \rightarrow Y$

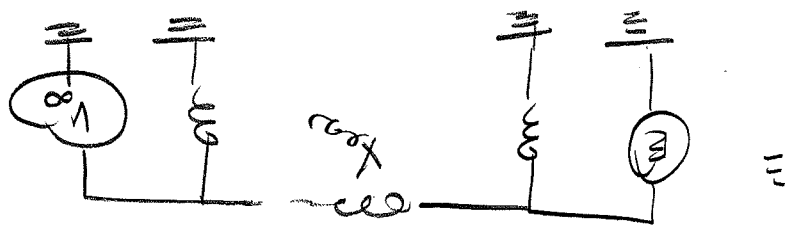


$$X_2 = \frac{0.3 \times 0.3}{0.3 + 0.3 + 0.14}$$

$$X_1 = 0.12$$

$$X_2 = 0.12$$

$$X_3 = 0.12$$



$$X_{e2} = \frac{0.5 \times 0.1 + 0.1 \times 0.1}{0.12}$$

with

$$X_{e2} = 1.1$$

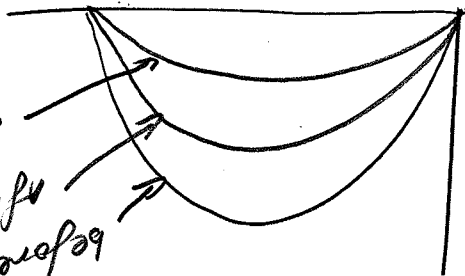
$$X_{e2} = (0.14)(0.3) + (0.3)(0.5) + (0.3)(0.3)$$

$$X_{e2} = 1.1 \text{ pu}$$

6) after clearing the fault with X_{e2} removed

$$X_{e3} = X_{f3} = 0.7 \text{ pu}$$

before $\Rightarrow X_{e3} = 0.7 \text{ pu}$
 during $\Rightarrow X_{e3} = 1.1 \text{ pu}$



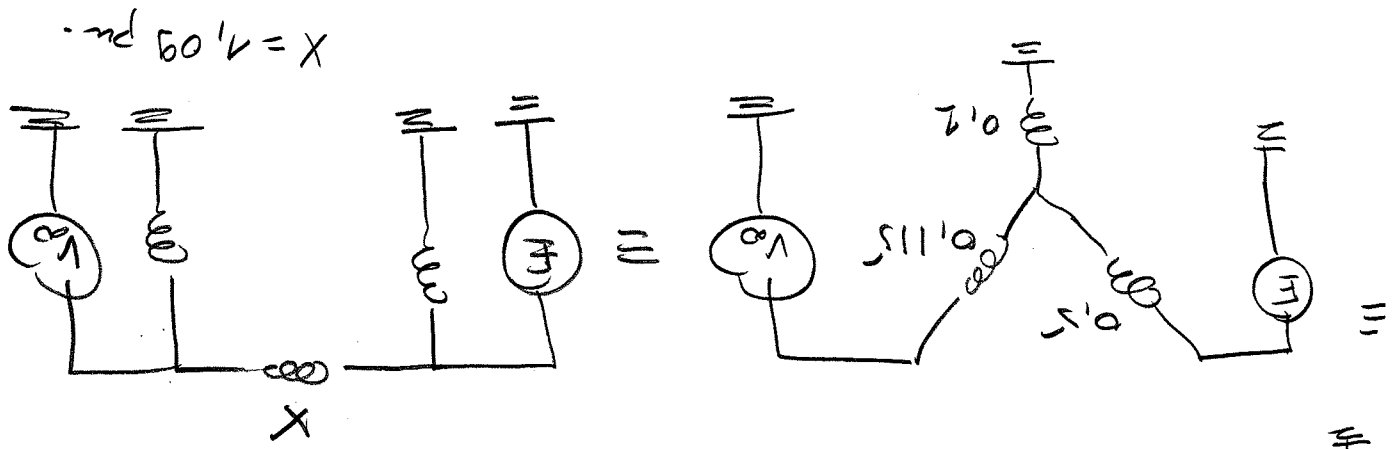
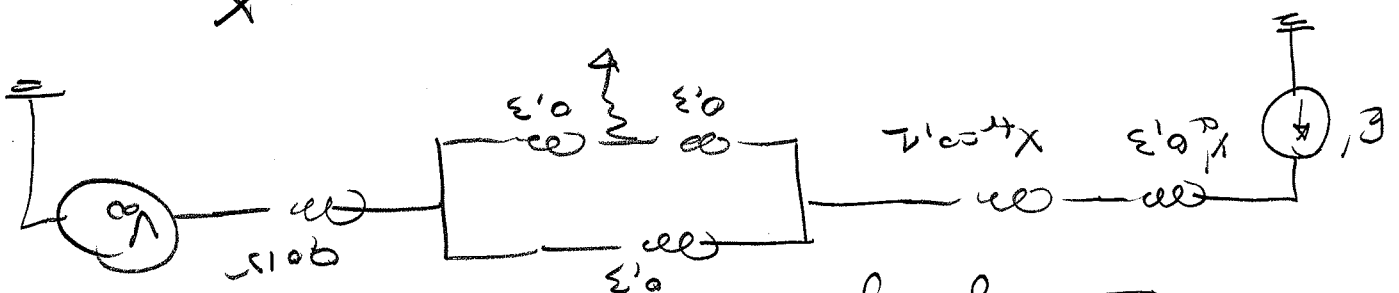
7)

1) It's a tendency of a power system to develop restoring forces equal to or greater than the disturbing forces to maintain the state of equilibrium as known as stability -

$$\frac{2H P \delta}{\omega_s dt^2} = P_m - P_e$$

$$\frac{4H^2 \delta}{\pi f_0 dt^2} = P_m - P_e$$

3) Leading angle

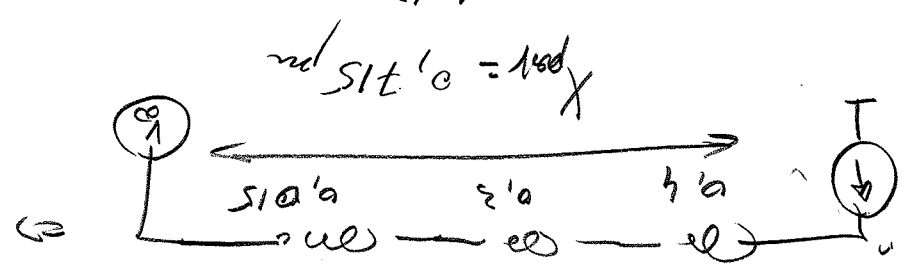


$X = 1.09 pu$

$$r_2 = \frac{P_{max2}}{P_{max}} = \frac{1,902}{1,636} = 0,860$$

$$r_1 = \frac{P_{max1}}{P_{max}} = \frac{1,902}{1,0} = 1,902$$

$$\Rightarrow P_{max2} = \frac{1,17 \times 1,0}{0,715} = 1,636 \text{ pu}$$



After fault

$$P_{max2} = \frac{\infty}{1,17/1,1} = 0,104$$

With X during fault $X = \infty$

$$P_{max2} \sin \delta_2 = \frac{X}{|E|/V} \sin \delta \Rightarrow$$

During fault

$$\Rightarrow \delta_0 = 24,86^\circ \approx 0,434 \text{ rad}$$

$$2) \quad 1,902 \sin \delta_0 = 0,8$$

$$P_{max} \sin \delta = P_e = \frac{X_{pre}}{|E|/V} \sin \delta = \frac{1,17/1,1}{0,615} \sin \delta = 0,8 \text{ with } P_{max} = 1,902$$

Before fault

$$E = 1,17 \angle 24,86^\circ$$

When the system critically stable

$$P_{max} \delta_{in} (\pi - \delta_m) = P_{max} \delta_o$$

$$\Rightarrow P_{max} \delta_{in} (\pi - \delta_m) = 0.8 = \pi \delta_m \Rightarrow \delta_{in} \left(\frac{\pi}{0.8} - 1 \right) = \frac{0.8}{\pi}$$

$$\delta_m = \pi - \left[\delta_{in} \left(\frac{\pi}{0.8} - 1 \right) \right]$$

$$\delta_m = 180^\circ - \delta_{in}$$

$$\delta_m = 150.7^\circ = 2.63 \text{ rad}$$

$$\cos \delta_o = \frac{0.860}{(2.63 - 0.434) [0.124, 88^\circ] - 0.000} \left[\cos 24.82^\circ + 0.86 \cos 150.7^\circ \right]$$

$$\cos \delta_o = \frac{0.860}{0.201} \Rightarrow \delta_o = 78.39^\circ$$

$$f_{ce} = \sqrt{\frac{2\pi (\delta_c - \delta_o)}{\pi f_o P_m}} = 1.37 \text{ rad}$$

$$= \sqrt{\frac{3.14 \times 0.50 \times 0.8}{(2 \times 4 \times (1.37 - 0.434))}}$$

$$f_{ce} = 0.244 \text{ sec}$$

$$P_e = \frac{X}{|E|V} \sin \delta = 1.17 \sqrt{2418664} \times 1\% = 1.07314 \sqrt{2418664} = 1.09$$

$$E = 1 + j + \sqrt{0.615} (\cdot 18 - j \cdot 17) = 1 + \sqrt{0.615} + j(1 - 17 \cdot \sqrt{0.615}) = 1.77 \sqrt{2418664}$$

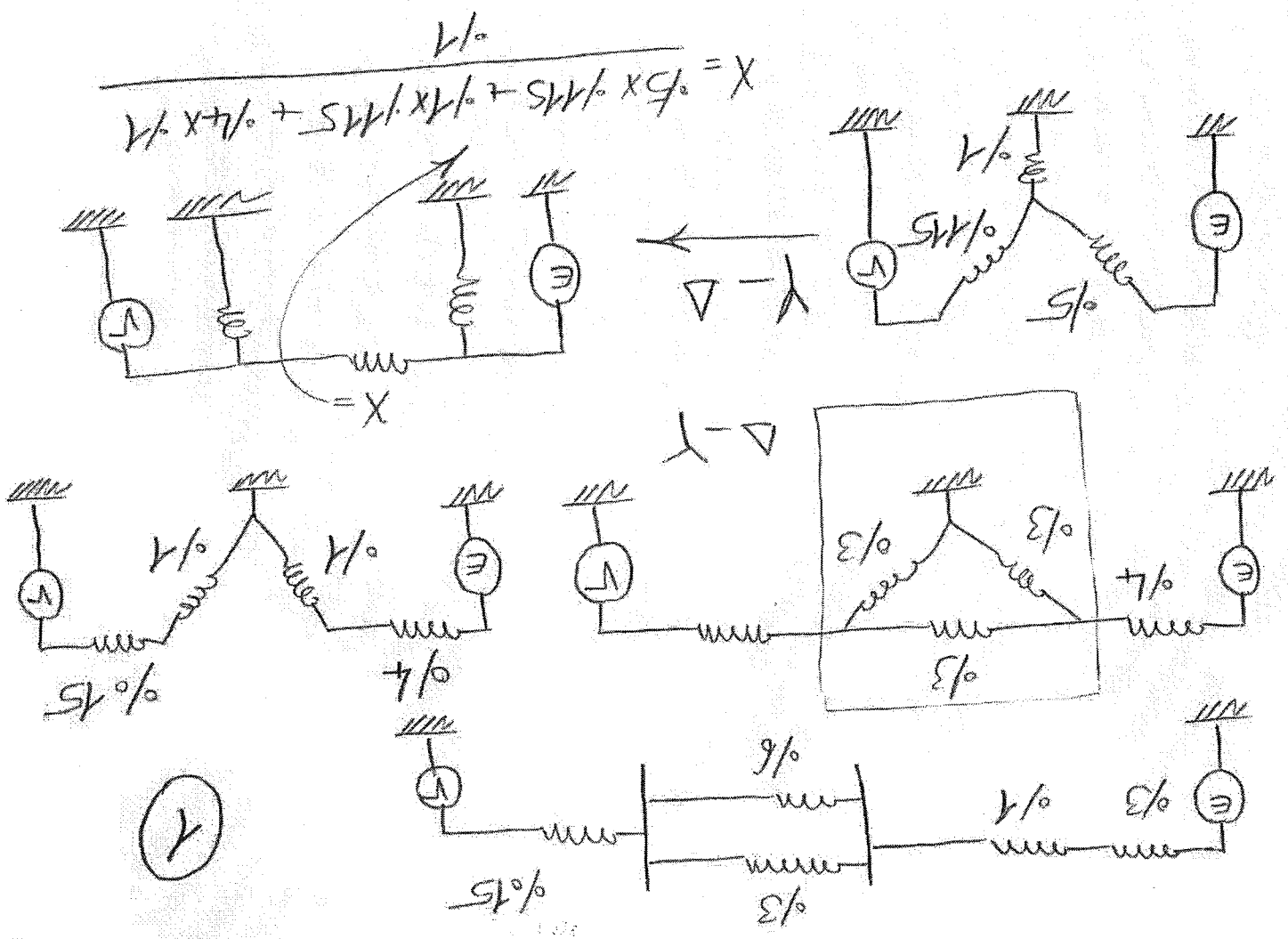
$$X = \frac{0.3 + 0.1}{0.3 \times 0.6} + \frac{0.15}{0.15} = \frac{0.4}{0.18} + 1 = 2.22 + 1 = 3.22$$

(before)

$$E = V + jXI$$

$$S = 0.8 + j \cdot 1 = V I^* \rightarrow I = 0.8 - j \cdot 1 = 1.28 \angle -51.34^\circ$$

During the fault $X = 1.09$



$$n=3 \quad \delta_2 = 39,0379$$

$$P_e(2) = 1,0734 \cdot \sin(39,0379) = 1,0446$$

$$P_a(2) = P_m - P_e(2) = 1 - 1,0446 = -0,0446$$

$$\Delta \delta_3 = \Delta \delta_2 + \frac{P_a(2)}{M} (\Delta t)^2 = -0,0446$$

$$\delta_3 = \delta_2 + \Delta \delta_3 = 39,0379 - 0,0446 = 38,9933$$

$$n=2 \quad \delta_1 = 28,4892$$

$$P_e(1) = 1,0734 \cdot \sin(28,4892) = -0,2289$$

$$P_a(1) = P_m - P_e(1) = 1 + 0,2289 = 1,2289$$

$$\Delta \delta_2 = \Delta \delta_1 + \frac{P_a(1)}{M} (\Delta t)^2 = 3,6292 + 6,1915 = 10,15487$$

$$\delta_2 = \delta_1 + \Delta \delta_2 = 28,4892 + 10,15489 = 39,0379$$

$$n=1 \quad \delta_0 = 24,186$$

$$P_e(0) = 1,0734 \cdot \sin(24,186) = -0,2891$$

$$P_a(0) = P_m - P_e(0) = 1 + 0,2891 = 1,2891$$

$$\Delta \delta_1 = \Delta \delta_0 + \frac{P_a(0)}{M} \Delta t \cdot \frac{\Delta t}{2} = 3,6292$$

$$\delta_1 = \delta_0 + \Delta \delta_1 = 24,186 + 3,6292 = 28,4892$$

$$M = \frac{180}{4} = \frac{180 \times 50}{4} = 4144,1 \text{ MJ} \cdot \text{s} / \text{deg}$$

(2)